

# Evaluation Method of Formation Ship-to-air Missile Air Defense Area Capability

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## Abstract

**Aiming at the problem of evaluating formation ship-to-air missile air defense area capability based on azimuth formation and herringbone formation, an evaluation method of formation ship-to-air missile air defense area capability was proposed, which can evaluate the formation ship-to-air missile air defense area capability indexes such as the maximum intercepting target times and the missile consumption, and provide a method basis for the formation ship-to-air missile air defense area capability evaluation.**

## Keywords

**Formation; Ship-to-air Missile; Air Defense; Area Capability.**

## 1. Introduction

When the ship-to-air missile weapon of the ship formation intercepts aerial targets, the formation ship-to-air missile air defense area capability evaluation can be studied. Prior methods, such as comprehensive analysis method [1-14], index method [15-17], simulation method [18-20], are primarily used for assessing ship-to-air missile air defense capability evaluation of single ship-to-air missile system. The factors such as area capability and formation type aren't considered by the above methods.

A method for evaluating the formation ship-to-air missile air defense area capability is proposed in this paper, which can be used to evaluate the formation ship-to-air missile air defense capability indexes such as the maximum intercepting target times and ship-to-air missile consumption, which provides a method and basis for the formation ship-to-air missile air defense area capability evaluation.

## 2. Evaluation Method of Formation Ship-to-Air Missile Air Defense Area Capability based on Azimuth Formation

As shown in Figure 1, it is assumed that the distance values of the ship-to-air missile horizontal plane launch areas of ships  $A_{f1}$ ,  $A_{f2}$ ,  $A_{f3}$  are all  $R_f$ . The  $Y_{f1}$  circle, the  $Y_{f2}$  circle, and the  $Y_{f3}$  circle are the ship-to-air missile horizontal plane launch areas of ships  $A_{f1}$ ,  $A_{f2}$ ,  $A_{f3}$  respectively. They are circles with the positions of ships  $A_{f1}$ ,  $A_{f2}$ ,  $A_{f3}$  as the center and the distance  $R_f$  as the radius. The intersections of the  $Y_{f1}$  circle and the  $Y_{f2}$  circle are points  $B_{f1}$  and  $B_{f2}$ , the intersections of the  $Y_{f2}$  circle and the  $Y_{f3}$  circle are points  $B_{f3}$  and  $B_{f4}$ , the intersections of the  $Y_{f1}$  circle and the array line are points  $C_{f1}$  and  $C_{f4}$ , the intersections of the  $Y_{f2}$  circle and the array line are points  $C_{f2}$  and  $C_{f5}$ , and the intersections of the  $Y_{f3}$  circle and the array line are points  $C_{f3}$  and  $C_{f6}$ .

In Figure 1. This paper mainly discusses the calculation of maximum intercepting target times defined by  $W_{fc}$  and maximum intercepting target missile consumption defined by  $W_{fd}$  when the target attacks in the ship-to-air missile cooperative horizontal launch area, a horizontal area composed of an arc segment  $B_{f3}C_{f5}B_{f4}$  and a straight segment  $B_{f3}B_{f4}$  of two adjacent ships, ship

$A_{f2}$  and ship  $A_{f3}$ . It is assumed that the target flies toward the ship  $A_{f2}$  at a constant speed in a straight line, and the angle between the target attack direction and the horizontal line is also a.

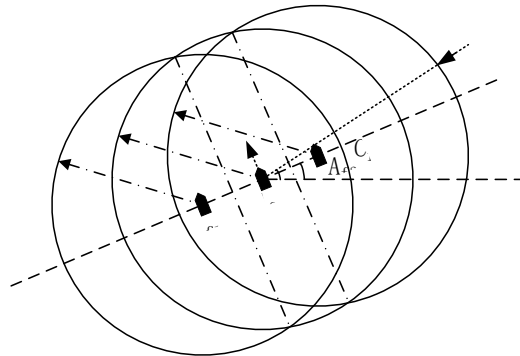


Figure 1. Azimuth formation

### 2.1. shoot-look-shoot (SLS)

Assume that the ship-to-air missile target encounter distance is  $S_{wd1}$  when the first ship-to-air missile launched by the ship intercepts the target. Suppose the reaction time of the ship-to-air missile weapon system is  $T_{fy}$ , the target speed is  $V_m$ , and the average speed of the ship-to-air missile is  $V_d$ . The calculation formula for  $S_{wd1}$  is in equation (1).

$$S_{wd1} = R_f - T_{fy} V_m - V_m [(R_f - T_{fy} V_m) / (V_m + V_d)] \tag{1}$$

The  $S_{wd1}$  value is valid when  $S_{wd1} \geq |A_{f2} D_{f2}|$ , and subsequent calculations are performed. The  $S_{wd1}$  value is invalid when  $S_{wd1} < |A_{f2} D_{f2}|$ , and no further calculations are performed.

Assume that the ship-to-air missile target encounter distance when the second ship-to-air missile launched by the ship intercepts the target is  $S_{wd2}$ , and the average time of ship-to-air missile damage effect evaluation is  $T_g$ , the launch time of ship-to-air missile system is  $T_b$ . The calculation formula for  $S_{wd2}$  is in equation (2).

$$S_{wd2} = S_{wd1} - T_g V_m - T_b V_m - V_m [(S_{wd1} - T_g V_m - T_b V_m) / (V_m + V_d)] \tag{2}$$

The  $S_{wd2}$  value is valid when  $S_{wd2} \geq |A_{f2} D_{f2}|$ , and subsequent calculations are performed. The  $S_{wd2}$  value is invalid when  $S_{wd2} < |A_{f2} D_{f2}|$ , and no further calculations are performed.

Assume that the ship-to-air missile target encounter distance when the third ship-to-air missile launched by the ship intercepts the target is  $S_{wd3}$ . The calculation formula for  $S_{wd3}$  is in equation (3).

$$S_{wd3} = S_{wd2} - T_g V_m - T_b V_m - V_m [(S_{wd2} - T_g V_m - T_b V_m) / (V_m + V_d)] \tag{3}$$

The  $S_{wd3}$  value is valid when  $S_{wd3} \geq |A_{f2} D_{f2}|$ , and subsequent calculations are performed. The  $S_{wd3}$  value is invalid when  $S_{wd3} < |A_{f2} D_{f2}|$ , and no further calculations are performed.

By analogy, assume that the ship-to-air missile target encounter distance is  $S_{wdN}$  when the  $N_{f1}$ th ship-to-air missile launched by the ship for the  $N_{f1}$ th time intercepts the target. Finally, when  $S_{wdN} < |A_{f2} D_{f2}|$ , the  $S_{wdN}$  value is invalid and the calculation is terminated. At this time,  $W_{fc} = N_{f1} - 1$  and  $W_{fd} = N_{f1} - 1$  are obtained.

### 2.2. shoot-shoot-look-shoot-shoot (SSLSS)

Calculation of the ship-to-air missile target encounter distance when the two missiles launched by the ship intercept the target for the first time. Among the two ship-to-air missiles this time, assume that the ship-to-air missile target encounter distance is  $S_{wd11}$  when the first ship-to-air missile intercepts the target. The calculation formula for  $S_{wd11}$  is in equation (4).

$$S_{wd11} = R_f - T_{fy} V_m - V_m [(R_f - T_{fy} V_m) / (V_m + V_d)] \tag{4}$$

The  $S_{wd11}$  value is valid when  $S_{wd11} \geq |A_{f2}D_{f2}|$ , and subsequent calculations are performed. The  $S_{wd11}$  value is invalid when  $S_{wd11} < |A_{f2}D_{f2}|$ , and no further calculations are performed.

Among the two ship-to-air missiles, assume that the ship-to-air missile target encounter distance is  $S_{wd12}$  when the second ship-to-air missile intercepts the target. Assume that the ship-to-air missile launch interval is  $T_j$ , the  $S_{wd12}$  calculation formula is in equation (5).

$$S_{wd12} = S_{wd11} - T_j V_m \tag{5}$$

The  $S_{wd12}$  value is valid when  $S_{wd12} \geq |A_{f2}D_{f2}|$ , and subsequent calculations are performed. The  $S_{wd12}$  value is invalid when  $S_{wd12} < |A_{f2}D_{f2}|$ , and no further calculations are performed.

Calculation of the ship-to-air missile target encounter distance when the two missiles launched by the ship for the second time intercept the target. Among the two ship-to-air missiles this time, assume that the ship-to-air missile target encounter distance is  $S_{wd21}$  when the first ship-to-air missile intercepts the target. The calculation formula for  $S_{wd21}$  is in equation (6).

$$S_{wd21} = S_{wd12} - T_g V_m - T_b V_m - V_m [(S_{wd12} - T_g V_m - T_b V_m) / (V_m + V_d)] \tag{6}$$

The  $S_{wd21}$  value is valid when  $S_{wd21} \geq |A_{f2}D_{f2}|$ , and subsequent calculations are performed. The  $S_{wd12}$  value is invalid when  $S_{wd21} < |A_{f2}D_{f2}|$ , and no further calculations are performed.

Among the two ship-to-air missiles, assume that the ship-to-air missile target encounter distance is  $S_{wd22}$  when the second ship-to-air missile intercepts the target. The calculation formula for  $S_{wd22}$  is in equation (7).

$$S_{wd22} = S_{wd21} - T_j V_m \tag{7}$$

The  $S_{wd22}$  value is valid when  $S_{wd22} \geq |A_{f2}D_{f2}|$ , and subsequent calculations are performed. The  $S_{wd22}$  value is invalid when  $S_{wd22} < |A_{f2}D_{f2}|$ , and no further calculations are performed.

By analogy, calculate the ship-to-air missile target encounter distance when the two ship-to-air missiles launched by the ship for the  $N_{f2}$ th time intercepting the target. Among the two ship-to-air missiles, assume that the ship-to-air missile target encounter distance is  $S_{wdN11}$  when the first ship-to-air missile intercepts the target, and the missile target encounter distance is  $S_{wdN12}$  when the second ship-to-air missile intercepting the target.  $S_{wdN11}$  and  $S_{wdN12}$  are calculated in the same way. First, if the value of  $S_{wdN11}$  is invalid when  $S_{wdN11} < |A_{f2}D_{f2}|$ , the subsequent calculation of  $S_{wdN12}$  is not performed, and  $W_{fc} = N_{f2} - 1$  and  $W_{fd} = 2(N_{f2} - 1)$  are obtained at this time. Second, if  $S_{wdN11} \geq |A_{f2}D_{f2}|$  and  $S_{wdN12} < |A_{f2}D_{f2}|$ , the  $S_{wdN12}$  value is invalid, and the calculation is terminated. At this time,  $W_{fc} = N_{f2}$ ,  $W_{fd} = 2(N_{f2} - 1) + 1$  is obtained.

### 3. Evaluation Method of Ship-to-Air Missile Air Defense Area Capability based on Herringbone Formation

As shown in Figure 2. Assume that the distance values of the ships  $A_{r1}$ ,  $A_{r2}$ ,  $A_{r3}$  and  $A_{r4}$  to the far end of the ship-to-air missile horizontal launch area are  $R_r$ , the straight lines  $A_{r1}J_{r1}$  and  $A_{r1}J_{r2}$  are the angle lines of the queue, and the straight line  $A_{r1}J_{r3}$  is the center line. The  $Y_{r1}$  circle, the  $Y_{r2}$  circle, the  $Y_{r3}$  circle, and the  $Y_{r4}$  circle are the ship-to-air missile horizontal launch areas of the ships  $A_{r1}$ ,  $A_{r2}$ ,  $A_{r3}$  and  $A_{r4}$  respectively. They are circles with the positions of the ships  $A_{r1}$ ,  $A_{r2}$ ,  $A_{r3}$ ,  $A_{r4}$  as the centers and the distance  $R_r$  of the ship-to-air missile horizontal launch areas of these ships as the radius. The intersections of the straight line  $A_{r1}J_{r3}$  and the circle  $Y_{r1}$  are points  $B_{r1}$  and  $B_{r4}$ , the intersections of the straight line  $A_{r1}J_{r3}$  and the circle  $Y_{r2}$  are points  $B_{r2}$  and  $B_{r5}$ , the intersections of the straight line  $A_{r1}J_{r3}$  and the circle  $Y_{r3}$  are points  $B_{r3}$  and  $B_{r6}$ , and the intersections of the straight line  $A_{r1}J_{r3}$  and the circle  $Y_{r4}$  are points  $E_{r1}$  and  $E_{r2}$ . The intersections of  $Y_{r1}$  circle and  $Y_{r2}$  circle are point  $D_{r1}$  and point  $C_{r3}$ , the intersections of  $Y_{r2}$  circle and  $Y_{r3}$  circle are point  $C_{r1}$  and point  $D_{r3}$ , the intersections of  $Y_{r1}$  circle and  $Y_{r3}$  circle are point  $C_{r2}$  and point  $D_{r3}$ , the intersections of  $Y_{r1}$  circle and  $Y_{r4}$  circle are point  $C_{r5}$  and point  $D_{r4}$ , and the intersections of  $Y_{r3}$  circle and  $Y_{r4}$  circle are point  $C_{r4}$  and point  $D_{r6}$ .

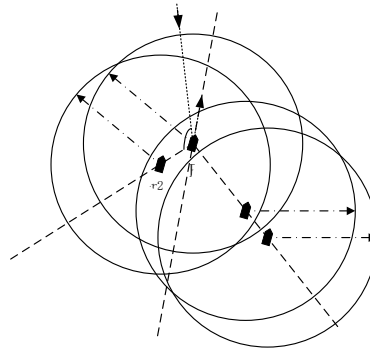


Figure 2. Herringbone formation

In Figure 2. This paper discusses the calculation of the maximum intercepting target times defined by  $W_{rc}$  and the maximum intercepting target missile consumption defined by  $W_{rd}$  when the target attacks in the ship-to-air missile cooperative horizontal plane launch area, a horizontal area composed of the arc segment  $\overline{B_{r2}D_{r1}D_{r2}D_{r4}B_{r4}}$  and the straight segment  $B_{r2}B_{r4}$  of two adjacent ships, ship  $A_{r1}$  and ship  $A_{r2}$ . It is assumed that the target is flying toward the ship  $A_{r1}$  in a constant speed straight-line flight. The included angle of the target's attack direction and the reference ship's port side queue angle line  $A_{r1}J_{r1}$  is  $C$ , and the intersection point of the target's attack direction line and the arc segment  $\overline{B_{r2}D_{r1}D_{r2}D_{r4}B_{r4}}$  is point  $F_{r1}$ . Let the ship spacing between two adjacent ships, the ship  $A_{r1}$  and the ship  $A_{r2}$ , be  $L_{r1}$ .

Assume that the minimum distance is  $S_{xmin}$  when the ship-to-air missile system intercepts the target. Assume that the near boundary distance of the kill zone of the ship-to-air missile is  $S_{min}$ , the  $S_{xmin}$  calculation formula is in equation (8).

$$S_{xmin} = S_{min} + T_{fy}V_m + V_m[S_{min}/(V_m + V_d)] \tag{8}$$

### 3.1. Shoot-look-shoot (SLS)

Assume that the ship-to-air missile target encounter distance is  $S_{rz1}$  when the first ship-to-air missile launched by the ship intercepts the target. In equation (9),  $S_{rz1}$  is calculated.

$$S_{rz1} = |A_{r1}F_{r1}| - T_{fy}V_m - V_m[ (|A_{r1}F_{r1}| - T_{fy}V_m) / (V_m + V_d) ] \tag{9}$$

The  $S_{rz1}$  value is valid when  $S_{rz1} \geq S_{xmin}$ , and subsequent calculations are performed. The  $S_{rz1}$  value is invalid when  $S_{rz1} < S_{xmin}$ , and no further calculations are performed.

Assume that the ship-to-air missile target encounter distance is  $S_{rz2}$  when the second ship-to-air missile launched by the ship intercepts the target. In equation (10),  $S_{rz2}$  is calculated.

$$S_{rz2} = S_{rz1} - T_gV_m - T_bV_m - V_m[ (S_{rz1} - T_gV_m - T_bV_m) / (V_m + V_d) ] \tag{10}$$

The  $S_{rz2}$  value is valid when  $S_{rz2} \geq S_{xmin}$ , and subsequent calculations are performed. The  $S_{rz2}$  value is invalid when  $S_{rz2} < S_{xmin}$ , and no further calculations are performed.

Assume that the ship-to-air missile target encounter distance is  $S_{rz3}$  when the third ship-to-air missile launched by the ship intercepts the target. In equation (11),  $S_{rz3}$  is calculated.

$$S_{rz3} = S_{rz2} - T_gV_m - T_bV_m - V_m[ (S_{rz2} - T_gV_m - T_bV_m) / (V_m + V_d) ] \tag{11}$$

The  $S_{rz3}$  value is valid when  $S_{rz3} \geq S_{xmin}$ , and subsequent calculations are performed. The  $S_{rz3}$  value is invalid when  $S_{rz3} < S_{xmin}$ , and no further calculations are performed.

By analogy, calculate the missile target encounter distance ( $S_{rzN}$ ) when the  $N_{r1}$ st ship-to-air missile launched by the ship for the  $N_{r1}$ th time intercepting the target. Finally, when  $S_{rzN} < S_{xmin}$ , the  $S_{rzN}$  value is invalid and the calculation is terminated. At this time,  $W_{rc} = N_{r1} - 1$  and  $W_{rd} = N_{r1} - 1$  are obtained.

### 3.2. shoot-shoot-look-shoot-shoot (SSLSS)

Calculation of the missile target encounter distance when the two missiles launched by the ship intercepted the target for the first time. Among the two ship-to-air missiles this time, assume that the ship-to-air missile target encounter distance is  $S_{rz11}$  when the first ship-to-air missile intercepts the target. The calculation formula for  $S_{rz11}$  is in equation (12).

$$S_{rz11} = |A_{r1}F_{r1}| - T_{fy}V_m - V_m[(|A_{r1}F_{r1}| - T_{fy}V_m)/(V_m + V_d)] \quad (12)$$

The  $S_{rz11}$  value is valid when  $S_{rz11} \geq S_{xmin}$ , and subsequent calculations are performed. The  $S_{rz11}$  value is invalid when  $S_{rz11} < S_{xmin}$ , and no further calculations are performed.

Among the two ship-to-air missiles, assume that the missile target encounter distance is  $S_{rz12}$  when the second ship-to-air missile intercepts the target. The calculation formula for  $S_{rz12}$  is in equation (13).

$$S_{rz12} = S_{rz11} - T_j V_m \quad (13)$$

The  $S_{rz12}$  value is valid when  $S_{rz12} \geq S_{xmin}$ , and subsequent calculations are performed. The  $S_{rz12}$  value is invalid when  $S_{rz12} < S_{xmin}$ , and no further calculations are performed.

Calculation of the missile target encounter distance when the two missiles launched by the ship for the second time intercept the target. Among the two ship-to-air missiles this time, assume that the ship-to-air missile target encounter distance is  $S_{rz21}$  when the first ship-to-air missile intercepts the target. The calculation formula for  $S_{rz21}$  is in equation (14).

$$S_{rz21} = S_{rz12} - T_g V_m - T_b V_m - V_m[(S_{rz12} - T_g V_m - T_b V_m)/(V_m + V_d)] \quad (14)$$

The  $S_{rz21}$  value is valid when  $S_{rz21} \geq S_{xmin}$ , and subsequent calculations are performed. The  $S_{rz21}$  value is invalid when  $S_{rz21} < S_{xmin}$ , and no further calculations are performed.

Among the two ship-to-air missiles, assume that the ship-to-air missile target encounter distance is  $S_{rz22}$  when the second ship-to-air missile intercepts the target. The calculation formula for  $S_{rz22}$  is in equation (15).

$$S_{rz22} = S_{rz21} - T_j V_m \quad (15)$$

The  $S_{rz22}$  value is valid when  $S_{rz22} \geq S_{xmin}$ , and subsequent calculations are performed. The  $S_{rz22}$  value is invalid when  $S_{rz22} < S_{xmin}$ , and no further calculations are performed.

By analogy, calculate the ship-to-air missile target encounter distance when the two ship-to-air missiles launched by the ship  $N_{r2}$  intercepted the target. Among the two ship-to-air missiles this time, assume that the ship-to-air missile target encounter distance is  $S_{rzN11}$  when the first ship-to-air missile intercepts the target, and the ship-to-air missile target encounter distance is  $S_{rzN12}$  when the second ship-to-air missile intercepts the target.  $S_{rzN11}$  and  $S_{rzN12}$  are calculated in the same way. First, if  $S_{rzN11}$  is less than  $S_{xmin}$ , the value of  $S_{rzN11}$  is invalid, and the subsequent calculation of  $S_{rzN12}$  is not performed. At this time,  $W_{rc} = N_{r2} - 1$  and  $W_{rd} = 2(N_{r2} - 1)$  are obtained. Second, if  $S_{rzN11} \geq S_{xmin}$ , and when  $S_{rzN12} < S_{xmin}$ , the  $S_{rzN12}$  value is invalid, and the calculation is terminated. At this time,  $W_{rc} = N_{r2}$ ,  $W_{rd} = 2(N_{r2} - 1) + 1$  is obtained.

## 4. Conclusion

When evaluating the formation ship-to-air missile air defense area capability, the formation ship-to-air missile air defense capability indexes such as the maximum intercepting target times and the ship-to-air missile consumption are evaluated, which provides a method and basis for the formation ship-to-air missile air defense area capability evaluation.

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